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Waste as Energy Source in EU Action Plan for the Circular Economy

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Investigations present that changes in municipal solid waste composition and properties correlate with the size and density of the municipal solid waste type, that mechanical pre-treatment including separation by weight and size can be useful for preparation of refuse derived fuel (RDF) material and solid recovered fuel (SRF) used for energy recovery. The authors determine the parameters of separated components of the coarse fraction (lower heating value, moisture, ash content, carbon, nitrogen, hydrogen, sulphur, chlorine, and metals), and assess their viability for the preparation of alternative fuel.

Keywords: waste to energy, circular economy, waste characterisation.

Introduction

Closing the loop – a European Union (EU) action plan for the Circular Economy for the first time was proposed by the European Commission to the European Parliament in December 2015 (EC, 2017a). Now the European Commission has adopted the Circular Economy Package, which includes revised legislative proposals on waste (EPRS, 2016). The legislative proposals on waste, adopted together with the action plan, include long-term targets to reduce landfilling and to increase preparation for reuse and recycling of key waste streams such as

municipal waste and packaging waste:

- the EU target for recycling 65% of municipal waste by 2030;
- the EU target for recycling 75% of packaging waste by 2030;
- a binding landfill target to reduce landfill to the maximum of 10% of municipal waste by 2030;
- a ban on landfilling of separately collected waste and main tools how to reach those targets.

When waste cannot be prevented or recycled, recovering its energy content is in most cases preferable to landfilling it, in both environmental and economic terms. 'Waste to energy' can, therefore, play a role and create synergies with the EU energy and climate policy, but guided by the principles of the EU waste hierarchy (EC, 2017b).

The use of separated organic part as a fuel can be considered as one of the solutions to reduce the amount of landfilled waste. Scientific research on alternative and renewable resources, including the use of waste for energy production, has over the past 15 years been developing rapidly worldwide (Beckmann et al., 2009; Sharma and McBean, 2009; Pohl et al., 2010; Rotter, 2011; Vounatsos, 2012). Investigations present that changes in municipal solid waste composition and properties correlate with the size and density of the municipal solid waste type, that mechanical pre-treatment including separation by weight and size can be useful for preparation of refuse derived fuel (RDF) and solid recovered fuel (SRF) material used for energy recovery.

Solid recovered fuel is fuel produced from non-hazardous waste in accordance with EU standards for SRF, especially EN15359. It is typically produced from municipal solid waste (MSW), industrial and commercial waste or construction and demolition waste (C&DW). RDF is a non-defined term and refers to waste that has not undergone proper processing and is not standardised; meanwhile, SRF is sampled and tested according to EU standards (ERFO, 2017).

The objective of the report is to evaluate the mechanical pre-treatment technology for unsorted municipal solid waste in Latvia and opportunities for the preparation of alternative fuel as RDF or SRF by carrying out the analysis of waste composition and properties. The authors determine the parameters of separated components (lower heating value, moisture, ash content, carbon, nitrogen, hydrogen, sulphur, chlorine, and metals), and assess their viability for the preparation of alternative fuel.

Materials and methods

Since municipal solid waste including household waste is heterogeneous, selective waste sampling was used

to obtain a reliable sample that would be representative of the average waste composition: each of the random truckloads specifically selected from known waste producers in a specific territory was selected at a landfill in a specific waste accumulation period. For samples taken selectively, it is considered that these samples are fully representative of the population, and the samples include all types of waste characteristic of the specific population. The waste sampling method was appropriate for the assessment of the morphological composition of municipal solid waste and was tested using standards LVS EN 14899:2011; LVS CEN/TR 15310-1:2007 (Arina and Orupe, 2012). The samples were taken during the four seasons analysing the waste collection routes so as to select a waste load (3 loads) that would be representative of the average waste composition in the territory. Each load was weighed and a representative waste sample was taken from each load with the grab method – approximately 20% of the load. Each sample was screened for an experimental study in special movable (reciprocating motion) screening equipment that consists of three screens placed horizontally. The screen mesh size (d) of the upper screen is 300x300 mm, the middle screen is 150x150 mm, and the bottom screen is 70x70 mm.

The experimental truckloads of the collected municipal waste were treated using two different separation lines: the linear star screen and the rotating drum screen sorting line (Arina and Orupe, 2013). There are facilities for mechanical shredding, screening and separation of metal in a mechanical pre-treatment centre using linear star screen equipment. The separation and reloading waste station with a rotating drum screener is equipped with a mechanical pre-shredder, a drum screener, a magnetic separator of metal, a manual sorting line, and a cutting mill.

The method of waste sampling after the separation of waste using mechanical sorting lines was selected in order to study the quantity, composition and properties of the sorted waste fractions, to assess their viability for RDF or SRF production.

To predict the waste composition after the use of waste screening equipment and to recover secondary-use materials and materials for RDF or SRF production, the following parameters for examples of the

coarse fraction from both lines were determined using the standards:

- _ moisture content (%) – LVS EN 15414-3:2011;
- _ net calorific value (MJ*kg⁻¹) – LVS EN 15400:2011;
- _ chlorine content (%) – LVS EN 15408:2011;
- _ sulphur content (%) – LVS EN 15408:2011;
- _ ash content (%) – LVS EN 15403:2011;
- _ content of trace elements (As, Ba, Be, Cd, Co, Cr, Cu, Hg, Mo, Mn, Ni, Pb, Sb, Se, Tl, V and Zn) – LVS EN 15411:2012;
- _ content of major elements (Al, Ca, Fe, K, Mg, Na, P, Si, Ti) – LVS EN 15410:2012;
- _ C, H, N content (%) – LVS EN 15407:2011;
- _ degradable organic carbon (DOC) (%) – LVS EN 13137:2005.

Results and discussion

The average data on the content of municipal waste entering two selected sorting lines and, after the sorting, content of coarse fractions are presented in the Table 1.

The pre-treatment using automatic separation lines reduces inorganic components of the coarse fraction as metals, glass and stones and rising organic part as paper, plastics, textile, rubber and leather. The separated fractions have a lower moisture content and a higher heating value. The main properties of coarse fractions from both lines are presented in Table 2.

Such materials after drying and crashing can be used as an energy source in cement kilns (Table 3) or as an energy source for co-incineration plants using biomass and SRF. The nature of SRF is summarised in three parameters: mercury (indicating environmental impact), chlorine (indicating technical behaviour) and net calorific value (indicating the performance) (Table 4).

Additional restrictions limiting the use of waste material for co-incineration kilns are connected with ash content. The ash from biomass burning can be used as a fertiliser, taking into account its content, but adding the waste or RDF, the content of heavy metals and other pollutants can overcome the stated limits. The analyses of ash from separated coarse fractions are presented in Table 5.

Table 1

Content of municipal solid waste (mass %) entering the sorting equipment and after treatment by a drum screener and a disc screener (coarse fractions)

Type of waste	Entering a drum screener, %	Entering a disc screener, %	Coarse fraction after pre-treatment by a drum screener, %	Coarse fraction after pre-treatment by a disc screener, %
1	2	3	4	5
Biological and fine (<20 mm)	59.0	69.8	26.6	3.9
Paper	5.7	2.7	25.8	39.5
Cardboard	4.3	3.4		
Plastic	11.5	10.1	24.8	38.7
Textile, rubber, leather	4.4	4.7	12.8	10.6
Other	1.7	0.8	2.7	4.1
Wood	2.2	0.25	5.3	1.1
Glass	5.5	5.4	0.4	0.2
Metal	1.3	1.3	0.7	1.5
Aluminium	2.3	0.4		
Tin	0.3	0.4		
Inert	1.9	0.9	1.3	0.4

Table 2

The mean values of the parameters of coarse fractions after a drum screener and a disc screener

Fraction	Moisture, %	Q_{net} , MJ*kg ⁻¹	Ash, %	Cl, %	S, %	N, %	C, %	H, %
1	2	3	4	5	6	7	8	9
Coarse fraction after a drum screener	33	14	13	0.7	0.4	0.3	46.1	5.9
Coarse fraction after a disc screener	34.7	15	13.2	0.95	0.2	0.2	4.8	7.1

Table 3

Material properties used as an energy source for Broceni Cement Kiln

Parameter	Unit	Value	Standards
1	2	3	4
Upper heating value UHV (dry basis)	MJ/kg	>22	CEN/TS 15400
Lower heating value LHV (as received)	MJ/kg	>16	CEN/TS 15400
Lower heating value LHV (dry basis)	MJ/kg	>20	CEN/TS 15400
Moisture (as received)	M.-%	< 25	CEN/TS 15414
Ash content (dry basis)	M.-%	< 15	CEN/TS 14775 CEN/TS 15403
Sulphur (dry basis)	M.-%	<1.0	CEN/TS 15408
Chlorine (dry basis)	M.-%	<0.8	CEN/TS 15408
Particle size	mm	50 x 50 x 5	CEN/TS15415
Bulk density (as received)	t/m ³	>0.180	

Table 4

The system of solid recovered fuel classification

Classification characteristic	Statistical measure	Unit	Classes				
			1	2	3	4	5
1	2	3	4	5	6	7	8
Net calorific value (NCV)	Mean	MJ/kg	≥25	≥20	≥15	≥10	≥3
Chlorine (Cl)	Mean	%	≤0.2	≤0.6	≤1.0	≤1.5	≤3
Mercury (Hg)	Median 80th percentile	Mg/MJ Mg/MJ	≤0.02 ≤0.04	≤0.03 ≤0.06	≤0.08 ≤0.16	≤0.15 ≤0.30	≤0.50 ≤1.00

Table 5

Chemical content of ash for coarse fractions after screeners

Element	Unit	Mean values of the coarse fraction after a disc screener	Mean values of the coarse fraction after a drum screener
1	2	3	4
Hg	mg kg ⁻¹	0.495	0.40
Cd	mg kg ⁻¹	0.82	0.66
Tl	mg kg ⁻¹	0.34	0.26
Br	M.-%	0.008	0.002
I	M.-%	0.0008	0.001
Sb	mg kg ⁻¹	8.62	2.90
As	mg kg ⁻¹	0.58	0.40
Cr	mg kg ⁻¹	13.37	23.76
Co	mg kg ⁻¹	6.02	6.60
Cu	mg kg ⁻¹	37.87	26.4
Pb	mg kg ⁻¹	21.46	9.24
Mn	mg kg ⁻¹	129.87	136
Ni	mg kg ⁻¹	9.79	5.28
Sn	mg kg ⁻¹	5.54	108
V	mg kg ⁻¹	14.42	13.2

Characterisation of alternative fuel derived from municipal solid waste

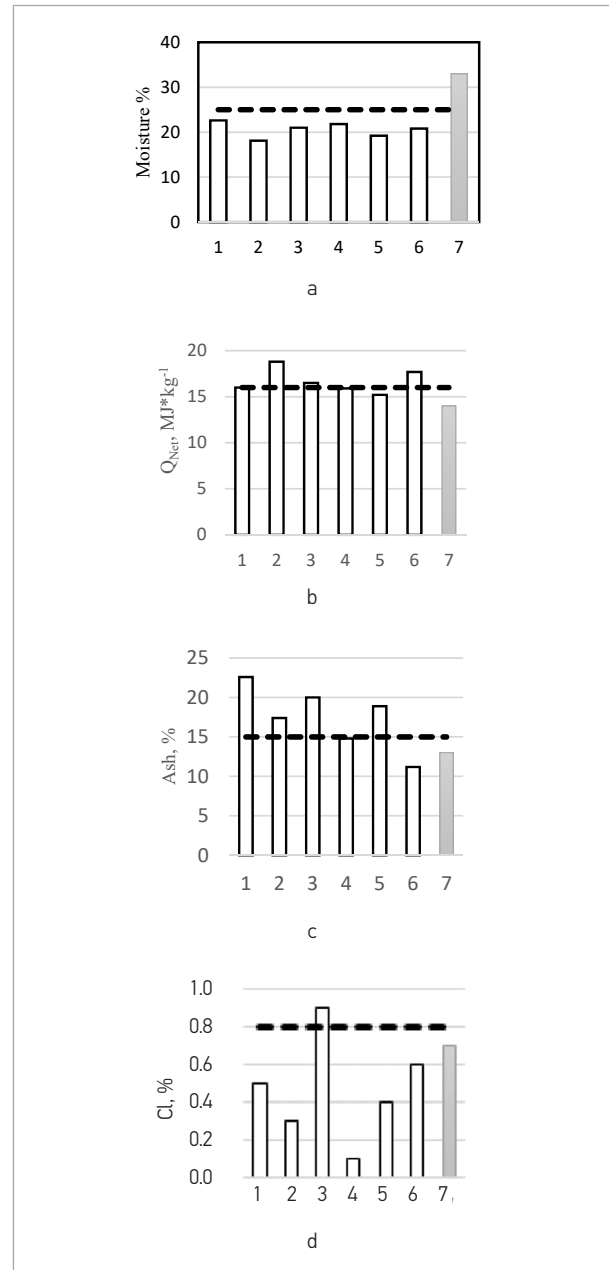
To improve the properties of sorted material according to the demands for usage as fuel for cement kiln, the mechanically sorted material (the coarse fraction after a drum screener) was mixed with manually sorted material (~20%). Figures a–d (Fig. 1) for six mixed samples (1–6) represent the data from the samples prepared by adding separately collected plastic and textiles and an output sample from the coarse fraction (7). The analyses of the main parameters indicate that the moisture content can be improved and the heat of combustion values can be increased by adding dry organic material.

The ash content meets the requirements of a high quality fuel only in some cases (examples 4 and 6).

The chlorine content corresponds to the limits for high quality fuel both in the coarse fraction and in the supplemented samples, except for sample 3 (exceeds the limit by 0.1%).

Fig. 1

Comparison of six mixed samples (1–6) and the coarse fraction sample (7) compared with the requirements for alternative fuel for cement kiln



Conclusions

- 1 The content of organic material in the mixed household waste can be raised by mechanical separation with disc or drum screeners. The coarse fraction after the separation process with a drum screener contains 25.8% of paper and cardboard (10% in the mixed waste), 24.8% of plastic (11.5% in the mixed waste), 12.8% of textile, rubber and leather (4.4% in the mixed waste). The coarse fraction after the separation process with a disc screener contains 39.5% of paper and cardboard (6.1% in the mixed waste), 38.7% of plastic (10.1% in the mixed waste), and 10.6% of textile, rubber and leather (4.7% in the mixed waste).
- 2 The mean energetic parameters for pre-treated mechanically sorted municipal waste respond to the limits stated for Class 3 of SRF. They are not available for cement kilns as the content of moisture is too high and the net calorific value is too low.
- 3 To improve the main characteristics of waste material after the separation of municipal waste on mechanical lines, manually sorted plastic and textile material can be added.
- 4 Biologically degradable waste separation at source and avoidance of hazardous materials containing chlorine and heavy materials are necessary to lower moisture, ash and chlorine content of potential fuel produced from waste.

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Energijos šaltinis iš komunalinių atliekų pagal ES veiksmo planą žiedinės ekonomikos kontekste

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Tyrimai rodo, kad komunalinių kietųjų atliekų sudėties ir savybių pokyčiai koreliuoja su komunalinių kietųjų atliekų rūšies dydžiu ir tankiu, kad mechaninis išankstinis apdorojimas, įskaitant atskyrimą pagal svorį ir dydį, gali būti naudingas ruošiant iš atliekų gautą kuro (RDF) medžiagą ir kietą regeneruotą kurą (SRF), kuris naudojamas energijos išgavimui. Autoriai nustato atskiras komunalinių atliekų frakcijos sudedamųjų dalių parametrus (mažesnę šilumos vertę, drėgmę, pelenų kiekį, anglį, azotą, vandenilį, sierą, chlorą ir metalus) ir įvertina jų gyvybingumą alternatyvaus kuro gamybai.

Raktiniai žodžiai: atliekos energijos šaltinis, žiedinė ekonomika, komunalinės atliekos.

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